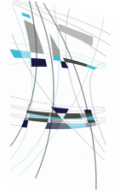


Ka-band compact multi-materials rectangular waveguide loads

Lab-STICC / UBO: *L. Martinez-Cano, A. Chevalier, A. Maalouf, J. Benedicto, P. Laurent, V. Laur*

IRDL / UBO: *J. Ville*

CNES: *K. Elis*



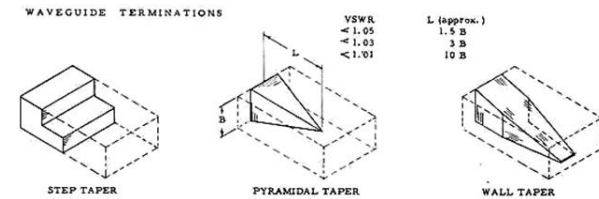
Plan

- ➔ **Technology and materials**
- ➔ **Design, fabrication and measurements**
 - ➔ Ka-band wedge loads
 - ➔ Ka-band compact loads
- ➔ **Conclusion and prospects**

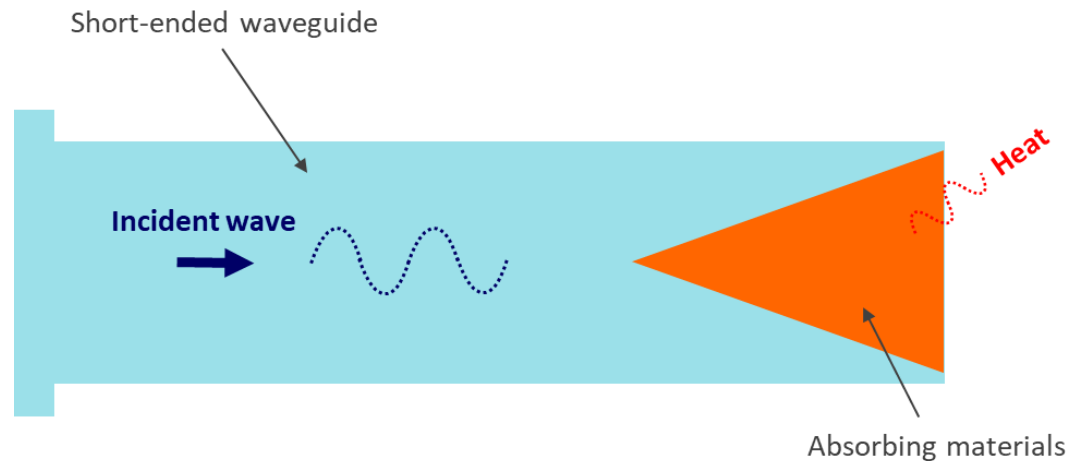
Technology and materials

➡ Microwave loads

- ➡ One port device
- ➡ Applications: isolators, couplers, metrology...
- ➡ Rectangular waveguide: short-ended waveguide + absorbers
- ➡ Characteristics: RL (or VSWR), Power Handling, BW, Size, Cost



Examples of absorber shape

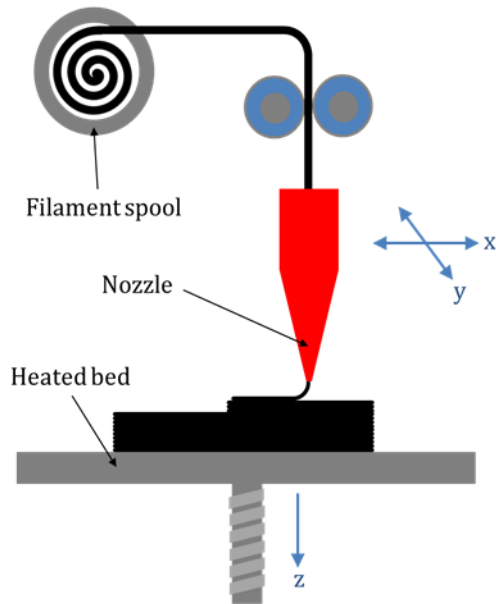


- **Additive technology: a low-cost way to shape absorbers**
- **R&T CNES activity: Case study ⇒ Compact WR-28 35.5-36 GHz loads / $S_{11} < -15$ dB**

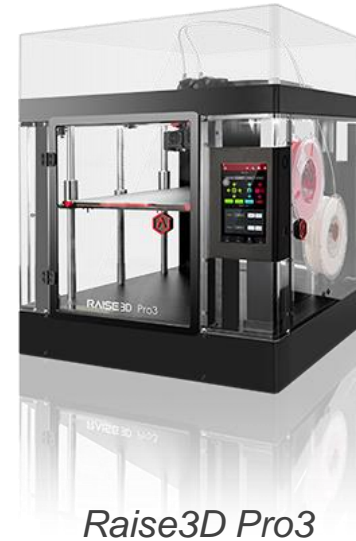
Technology and materials

➤ Fused Deposition Modeling

- Layer-by-layer deposition of a fused polymer
- Thickness of layer: 50 to 200 μm



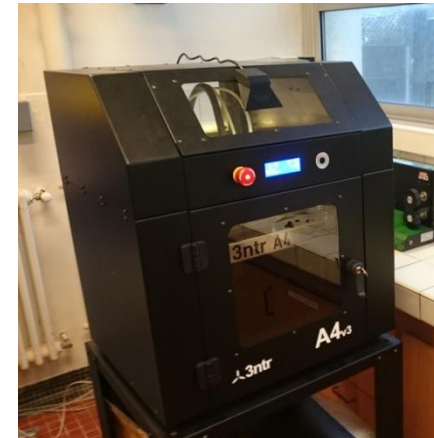
FDM principle



Raise3D Pro3



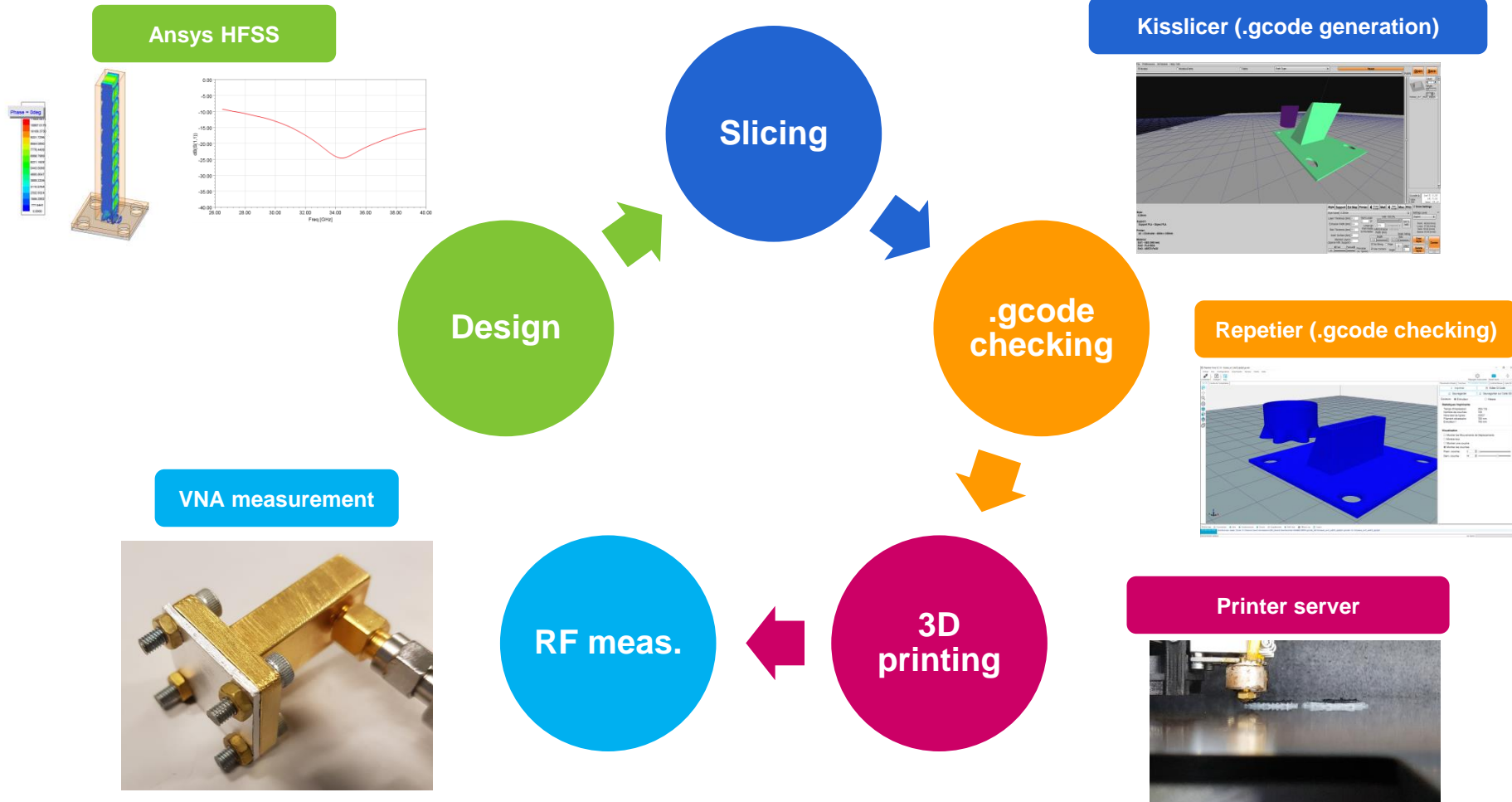
APIUM P155



3NTR A4 & A2

Technology and materials

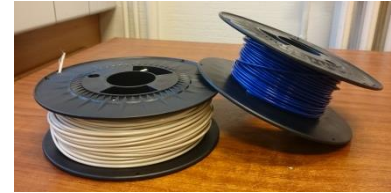
➡ From simulation to printed device: a simple and fast process



Technology and materials

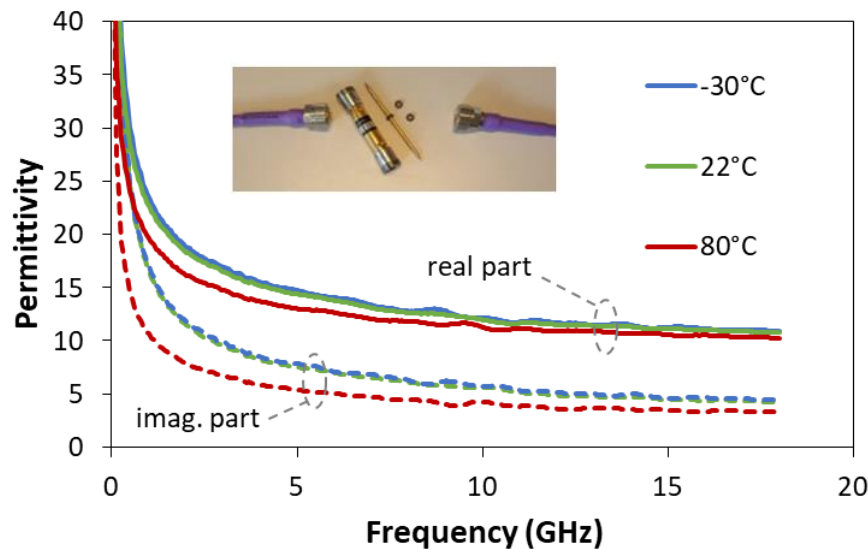
➤ Printable materials

- A lot of commercial references (mainly ABS, PLA)
- Pure polymers not of interest (low to medium losses)
- Composite materials (carbon, ferromagnetic particles): potential candidates for microwave absorption



➤ **Selected material: ABS-ESD (Nanovia)**

➤ **3D printers: 3NTR A4 and A2**



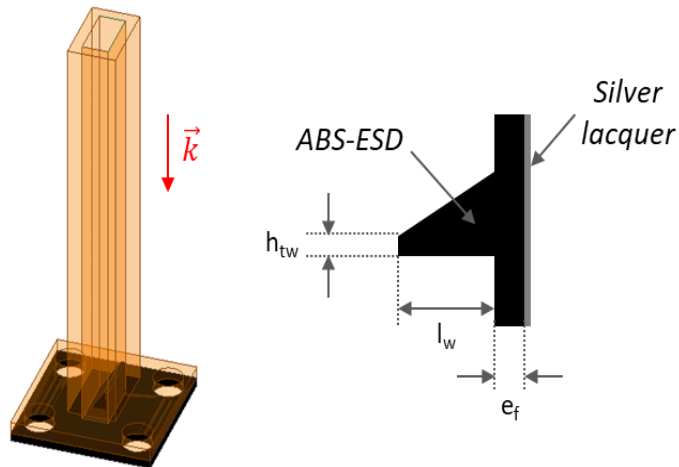
EM properties of ABS-ESD

- **EM properties: standard coaxial line method**
- **Decrease of permittivity at high temp.**
- **Ka-band (26-40 GHz):**
 - $\epsilon_r = 8$
 - $\tan\delta = 0.3$

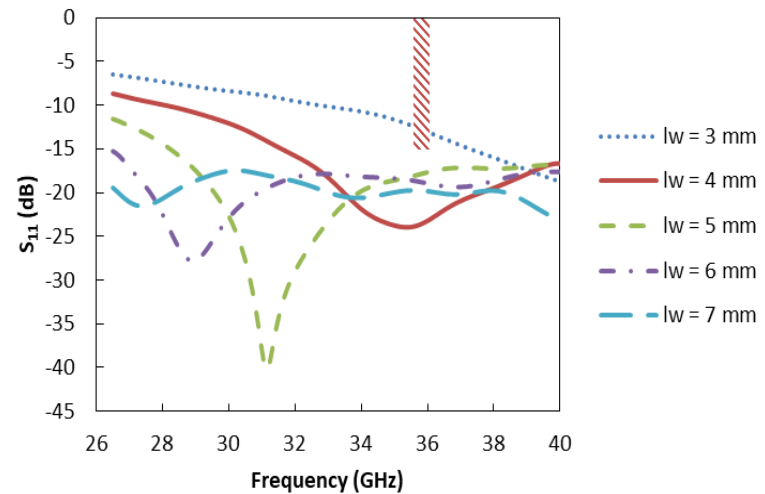
Design, fabrication and measurements

➤ Ka-band wedge loads

- Compatible with WR-28 RWG
- With integrated UBR 320 / IEC 60154 flange
- Metallized back face (silver lacquer $\sigma = 5 \cdot 10^6$ S/m)



Simulation model



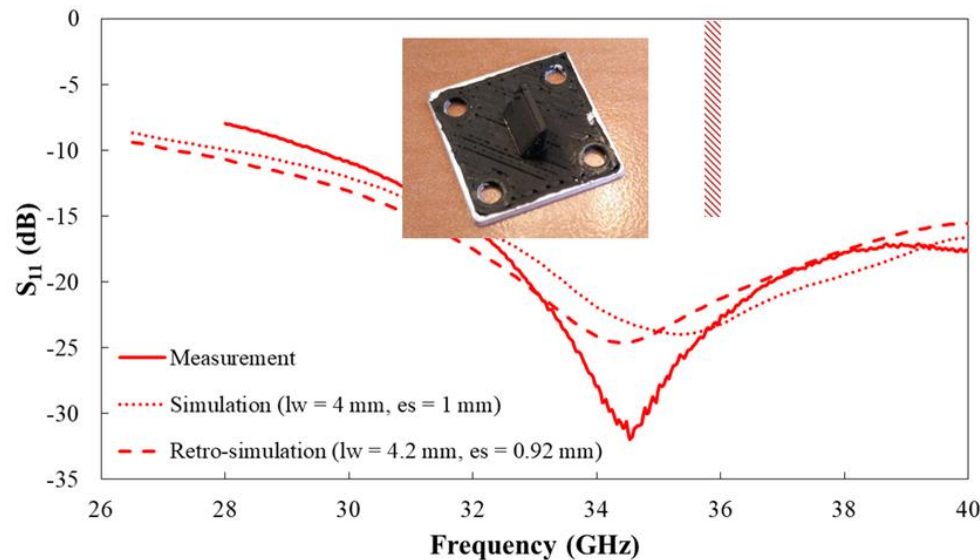
*Simulated reflection coefficient for different l_w
($h_w = 0.6$ mm, $e_f = 1$ mm)*

- Frequency of maximum absorption decreases when l_w increases
- Specifications achieved for $l_w = 4$ mm (total length 5 mm)

Design, fabrication and measurements

➤ Ka-band wedge loads

- 3D printed using a A4V3 printer (5 min.)
- Silver lacquer on back face (60°C / 1h)
- VNA measurement of S-parameters



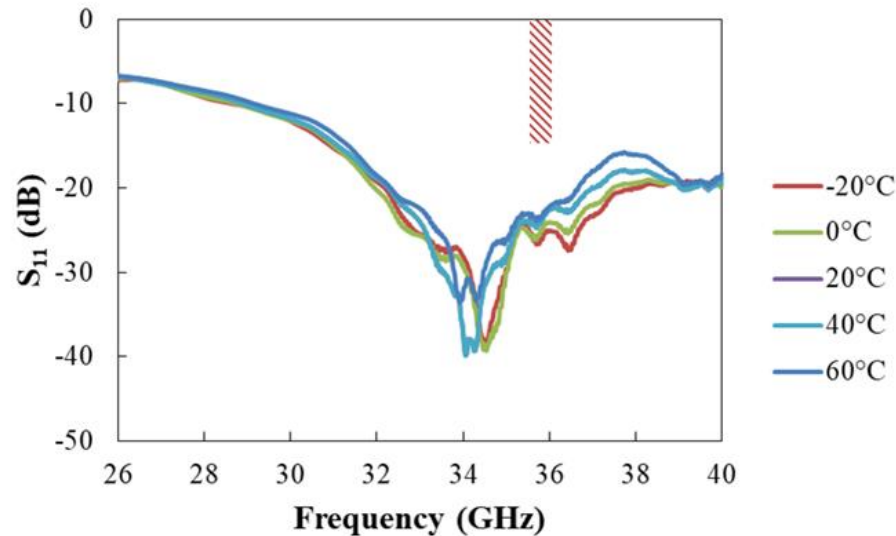
Comparison between simulated, measured and retro-simulated S-parameters

- Specifications achieved BUT 700 MHz frequency shift between simulated and measured S_{11}
- Real dimensions: $l_w = 4.2$ mm and $e_f = 0.92$ mm) \Rightarrow Better agreement

Design, fabrication and measurements

➤ Ka-band wedge loads

➤ Characterization between -20°C and +60°C



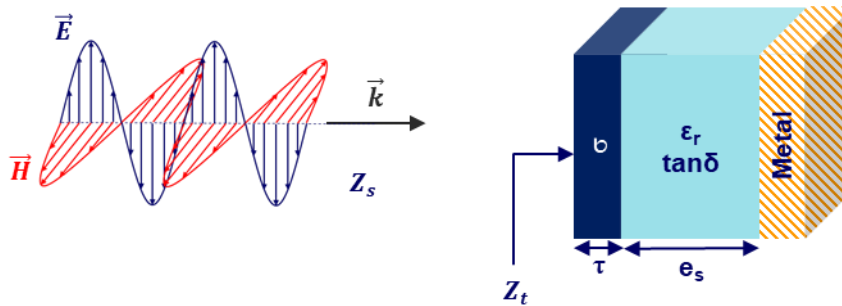
Measured S_{11} in Ka-band between -20°C and +60°C

- Slight increase at high temperature between 37 GHz and 38.5 GHz
- Specifications achieved in this temperature range

Design, fabrication and measurements

➡ Ka-band compact loads

➡ Multi-materials topology based on a Salisbury screen principle (dielectric spacer + resistive sheet)



Salisbury screen principle in free space

- **ABS: dielectric spacer $\Rightarrow \lambda_g/4 = 1.59$ mm at 36 GHz**
- **ABS-ESD: alternative to resistive sheet ($\tau = 0.1$ mm)**

Design equations for RWG

TE_{10} cutoff frequency

$$f_c = \frac{c}{2a}$$

TE_{10} impedance

$$Z_S = \frac{\sqrt{\frac{\mu_0}{\epsilon_0}}}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$

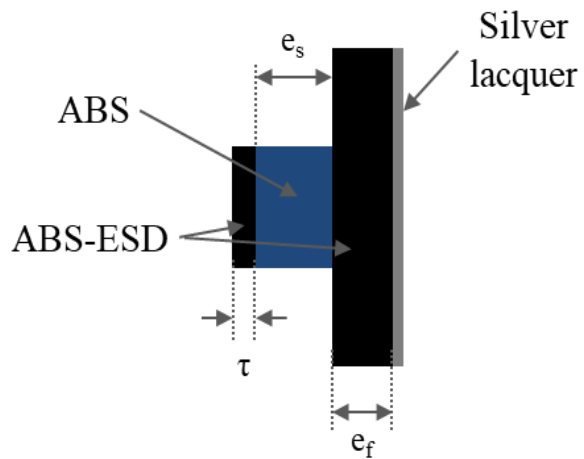
TE_{10} guided wavelength

$$\lambda_g = \frac{c}{f \sqrt{\epsilon_r} \sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$

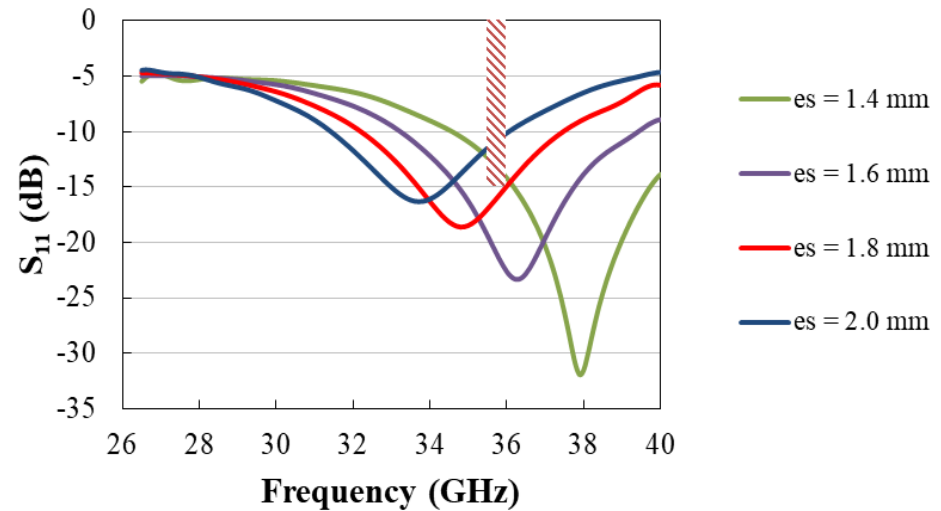
Design, fabrication and measurements

➡ Ka-band compact loads

- ➡ Design of multi-materials compact loads
- ➡ With integrated flange (ABS-ESD)



Side view of the compact load



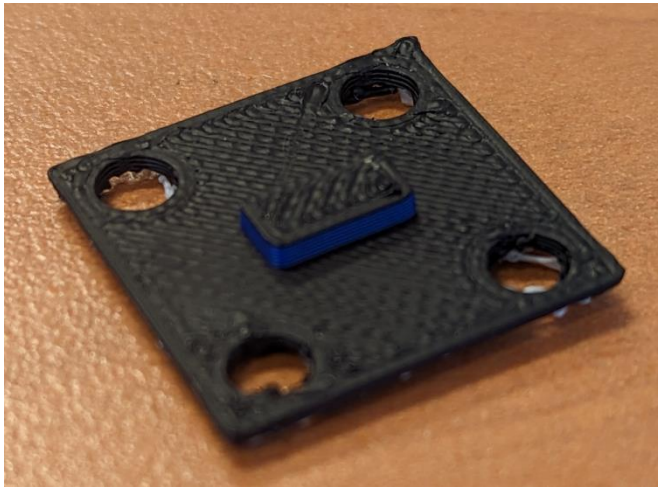
Simulated S_{11} in Ka-band for different spacer thickness

- Frequency of maximum absorption decreases from 37.9 GHz to 33.7 GHz for $1.4 \text{ mm} < e_s < 2 \text{ mm}$
- Specifications achieved for $e_s = 1.6 \text{ mm}$ (total length 2.7 mm)

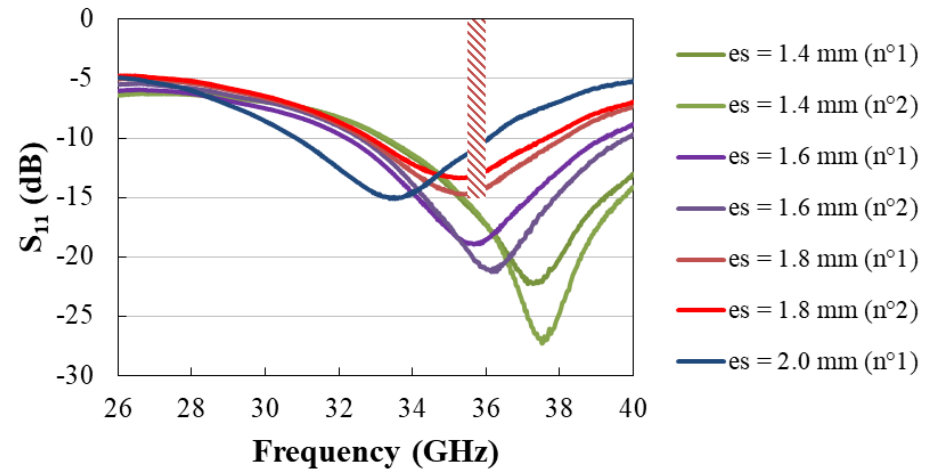
Design, fabrication and measurements

➡ Ka-band compact loads

- ➡ 3D printed using a A4V3 printer (3 min.)
- ➡ Silver lacquer on back face (60°C / 1h)



3D printed multi-materials load



Measured S_{11} in Ka-band for different spacer thickness

- **Good agreement between simulated and measured S_{11}**
- **Quite good reproducibility for two samples**
- **Specifications achieved for a total length of 2.7 mm \Rightarrow Reduction of 47% / standard topology**



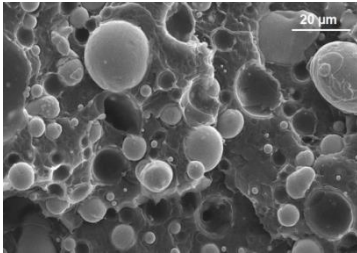
Conclusions and prospects

- FDM technology: promising low-cost, fast and easy-to-use technology for the fabrication of microwave load
 - Several commercial printable composite materials with appropriate EM properties
 - Useable up to 40 GHz and more...
 - Multi-materials topologies: decrease of size and weight
-
- **Technology limitations:**
 - Is it compatible with space applications ? Not using ABS matrix
 - Spatialization of this technology requires to study/develop new materials ⇒ R&T CNES 2

Conclusions and prospects

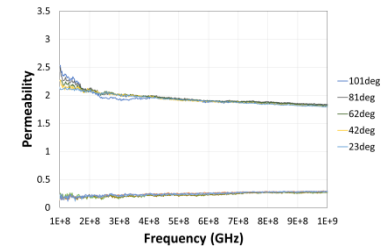
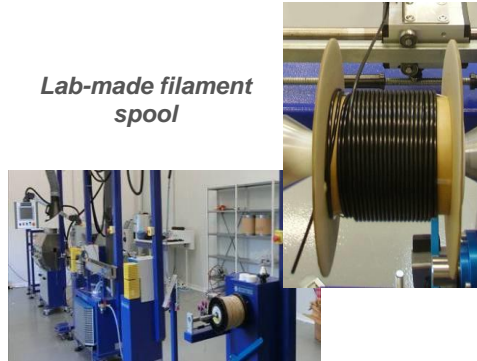
➤ High temperature materials

➤ Development of PEKK or PPS composites

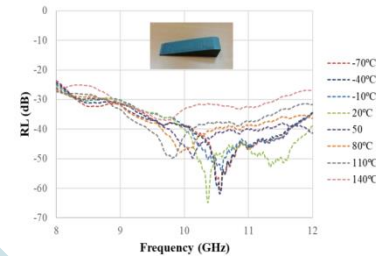


MEB picture of carbonyl iron/PPS composite

Lab-made filament spool



EM properties and S_{11} of a wedge loads



Composites elaboration

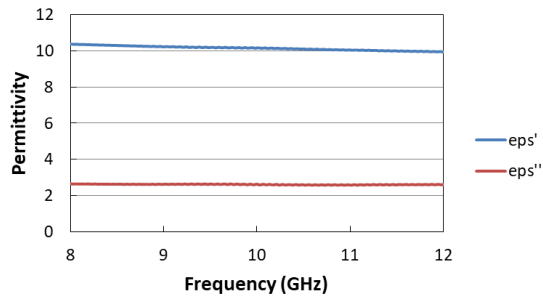
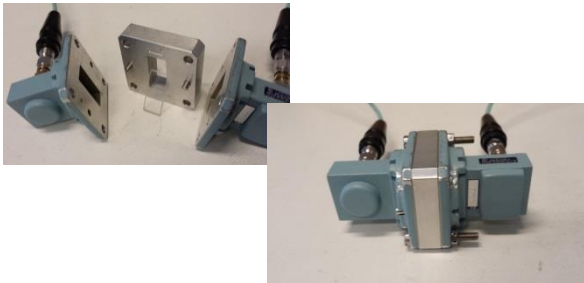
Filament extrusion

3D printing and evaluation

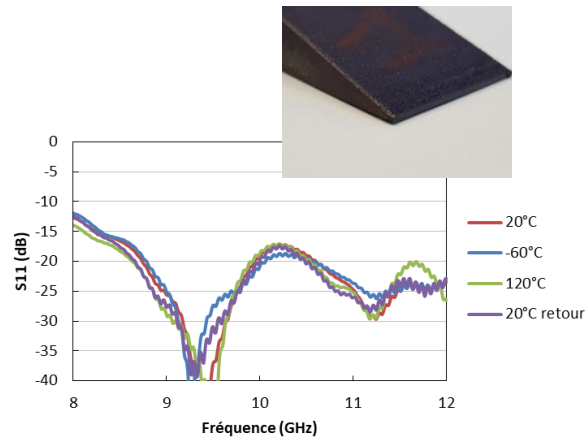
Conclusions and prospects

➤ High temperature materials

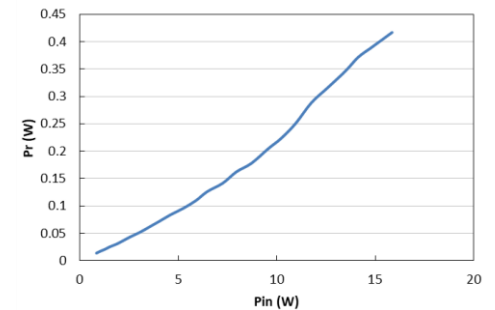
- Characterization and evaluation of commercial PPS, PEEK, PEKK composites



X-band characterization of a carbon-filled PEKK filament



Temperature stability of a carbon-filled PEKK wedge load



PHC evaluation of a carbon-filled PEKK wedge load



Acknowledgements

R&T CNES

« Apport des technologies additives pour la miniaturisation de charges hyperfréquences »



Thank you for your attention