

# Low-loss millimeter-wave self-biased circulators: materials, design and characterization

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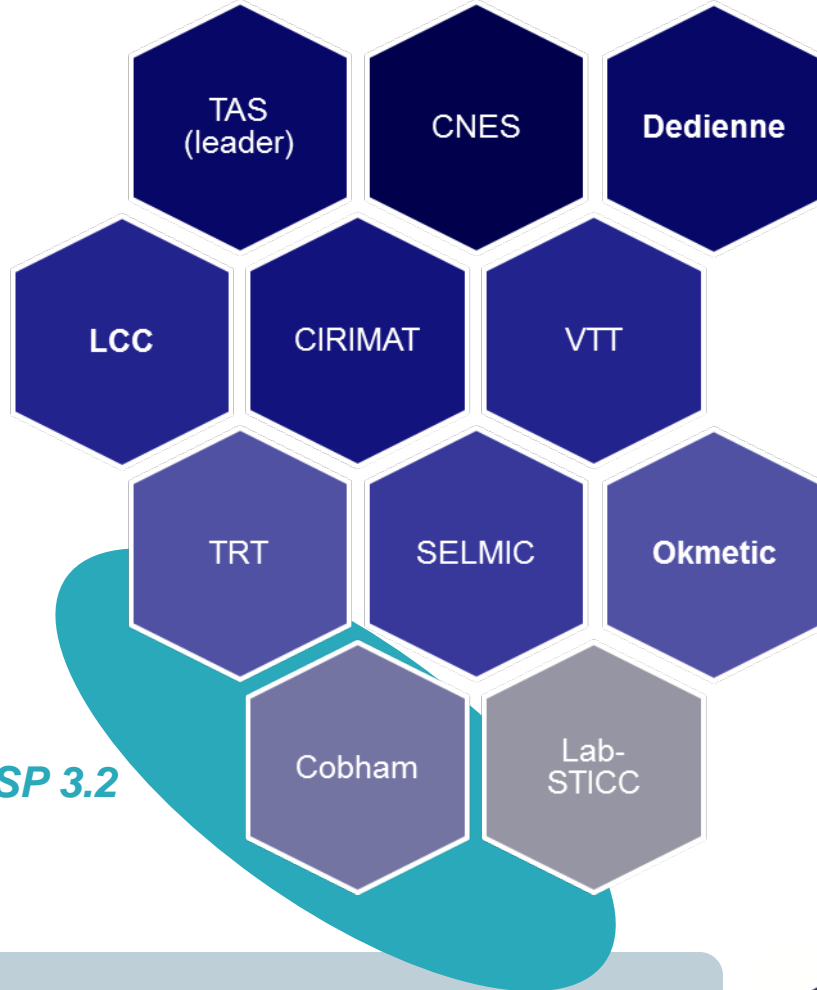
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## ➔ Advanced Millimeter Wave Interconnects



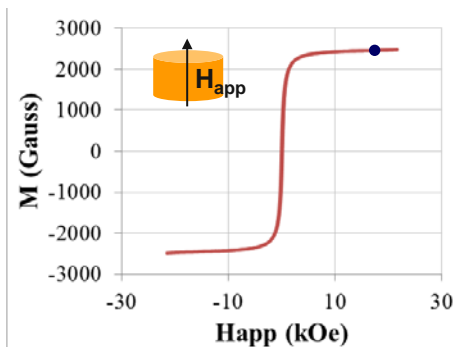
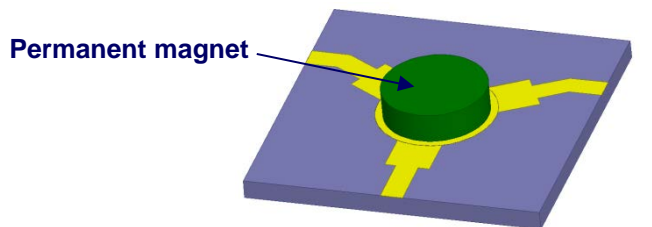
SP 3.2

### SP 3.2 Minaturized Self-biased Circulators

- Development of new pre-oriented materials for mm-wave applications (up to 40 GHz)
- Static and dynamic characterization of pre-oriented polycrystalline hexaferrites
- Proof of concept : rectangular waveguide mm-wave self-biased circulator
- Ultra-compact planar self-biased circulators
- Integration into RF front-end

# Self-biased circulators

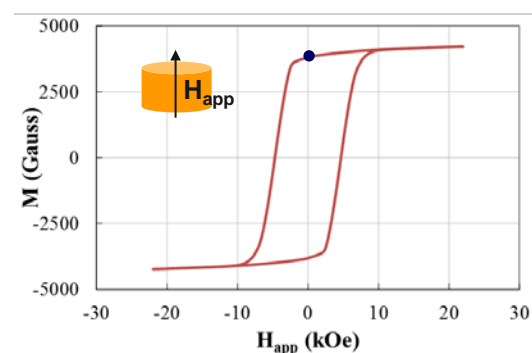
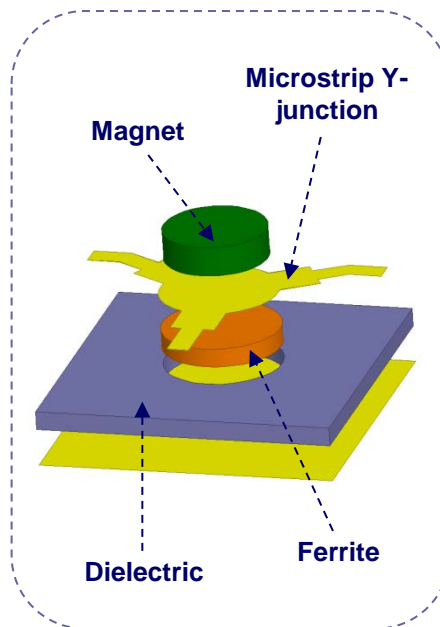
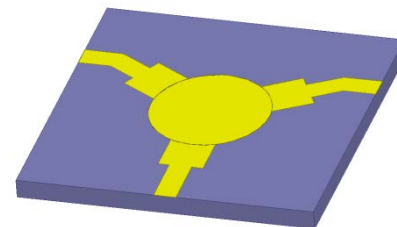
## Classical circulator



*Hysteresis cycle of a soft ferrite*

- Soft ferrite
- Magnetization state: saturation
- Need a permanent magnet

## Self-biased circulator

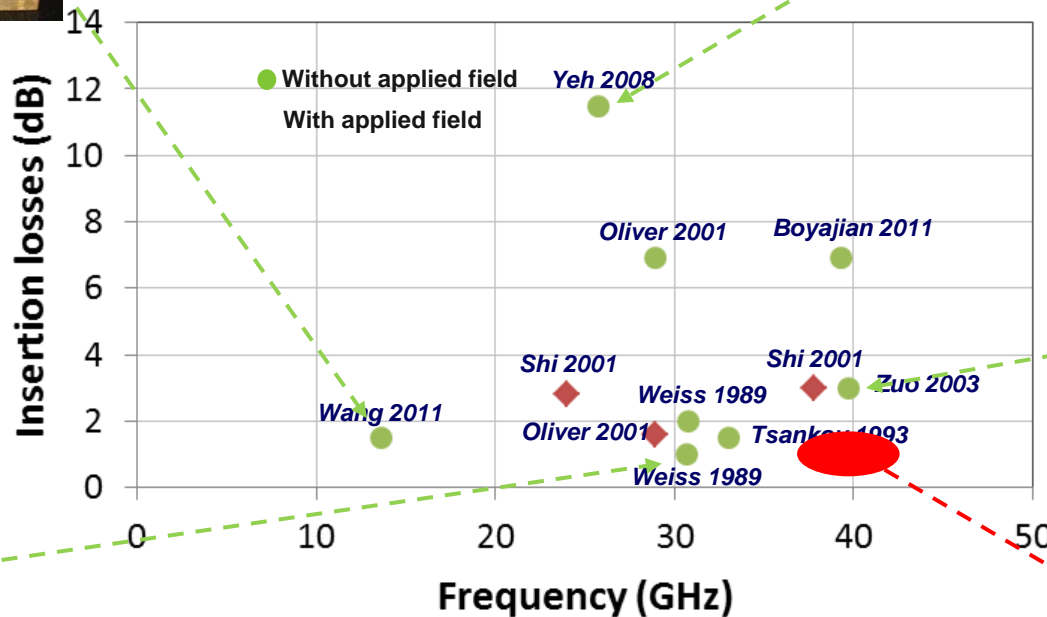
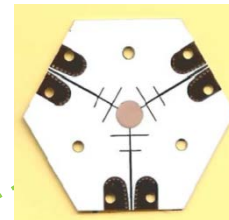
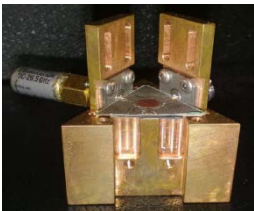


*Hysteresis cycle of a pre-oriented hexaferrite*

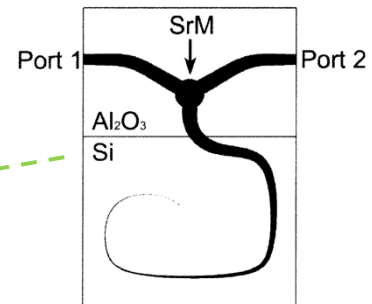
- Pre-oriented hexaferrite
- Magnetization state: remanence
- No permanent magnet
- Easier integration

# Self-biased circulators

## State of the art



Insertion losses as a function of frequency measured for hexaferrite-based circulators



Difficult to address (proximity of GMR)

# Self-biased circulators

## ➔ Choice of materials

### ➤ Single crystal hexaferrites

- ☺ *High anisotropy field (compatible with mm-wave applications)*
- ☺ *Low  $\Delta H$*
- ☹ *Low remanent magnetization (permanent magnet needed)*

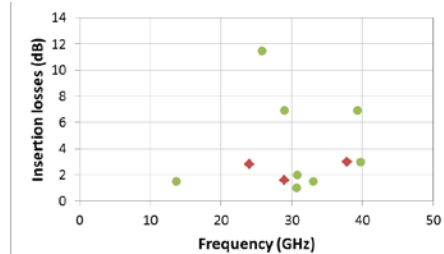
### ➤ Pre-oriented hexaferrite composites

- ☺ *High anisotropy field (compatible with mm-wave applications)*
- ☺ *High remanent magnetization (self-biased working mode)*
- ☹ *High  $\Delta H$  (porosity)*
- ☹ *High  $\tan\delta_d$  (use of organic binder)*

### ➤ Polycrystalline pre-oriented hexaferrites (mainly BaM and SrM)

- ☺ *High anisotropy field (compatible with mm-wave applications)*
- ☺ *High remanent magnetization (self-biased working mode)*
- ☹ *Moderate  $\Delta H$  (porosity)*

➔ Use of SrM with La,Co substitution to increase anisotropy field



# Hexaferrites

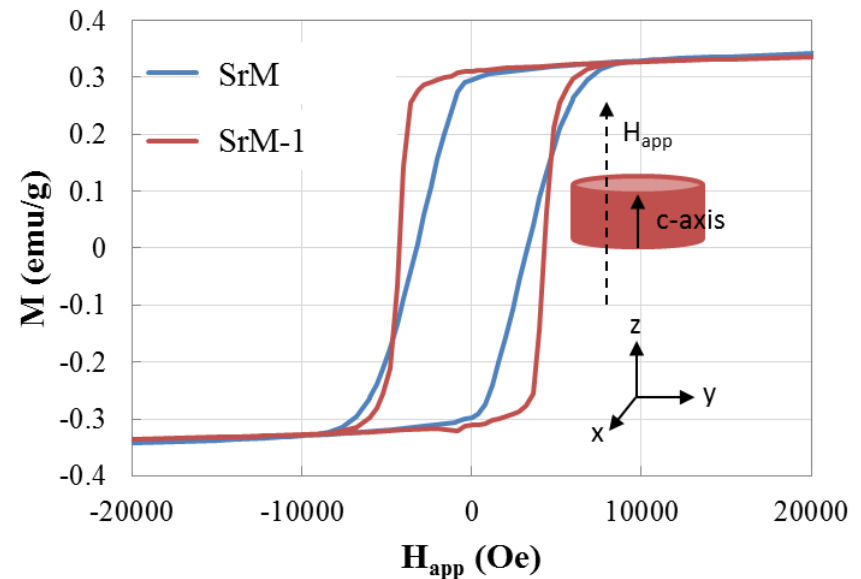
➤ **Materials: Substituted strontium hexaferrites (called SrM-1 and SrM-2)**

## ❑ **Synthesis:**

- Powder preparation (solid state reaction)
- Powder calcination
- Orientation during pressing
- Sintering at high temperature

## ❑ **Effects of substitution:**

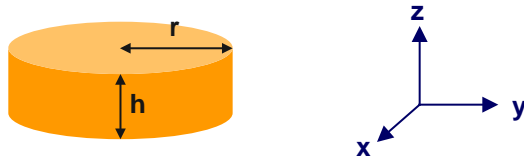
- Increase of  $M_r/M_s$
- Increase of  $H_k$  (higher working frequency / pure SrM)



*Comparison of SrM and SrM-1 hysteresis cycles measured using a SQUID*

# Hexaferrites

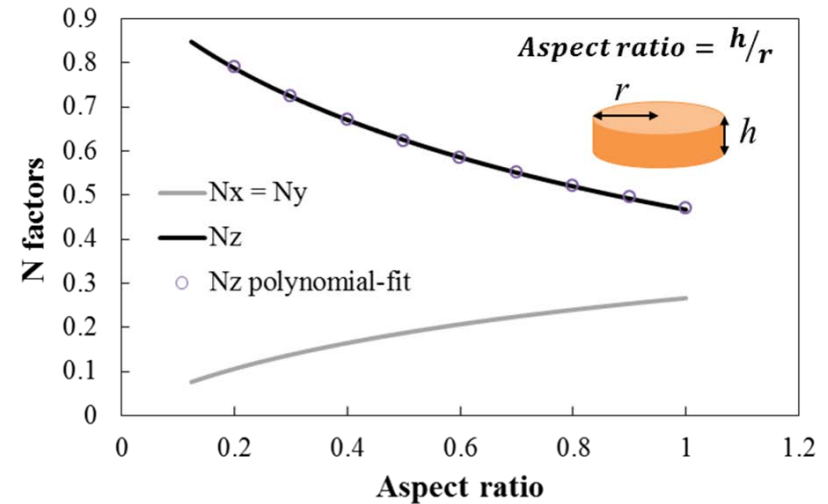
## ➤ Extrinsic properties of hexaferrite pucks



### ➤ Internal field

$$\vec{H}_{int} = \vec{H}_k + \vec{H}_{app} - \vec{N} \times \vec{M}$$

$$\text{with } \vec{N} = \begin{pmatrix} N_x & 0 & 0 \\ 0 & N_y & 0 \\ 0 & 0 & N_z \end{pmatrix}$$



Evolution of demagnetization coefficients as a function of aspect ratio

- Interpolation of  $N_z$  as a function of shape factor + integration into EM simulators
- Shape-dependant magnetic properties: taken into account during the simulations

# Modeling of circulators

- Use of Ansys HFSS and CST Microwave Studio softwares (Polder's model => only valid for fully saturated ferrites)
- Use of Polder's model for highly pre-oriented hexaferrites:

$$H_{int\ Polder} = H_{app} + H_A - N_z \times M_r \quad M_{Polder} = M_r$$

## Polder's model

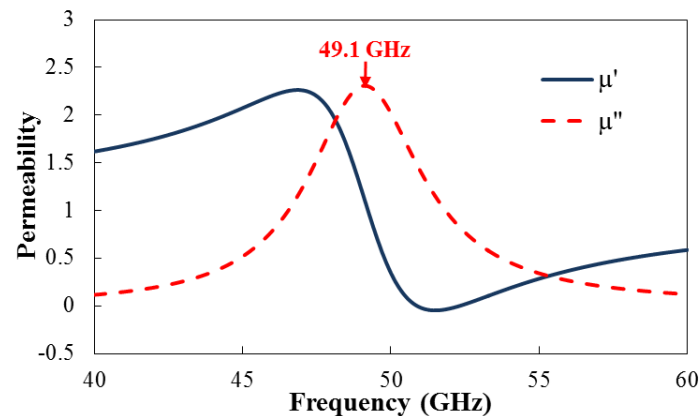
$$\mu = 1 + \frac{\omega_H \omega_M}{\omega_H^2 - \omega^2}$$

$$\kappa = \frac{\omega \omega_H}{\omega_H^2 - \omega^2}$$

$$\omega_H = \gamma(H_{int} + i\Delta H)$$

$$\omega_M = \gamma \cdot 4\pi M_z$$

$$\gamma = 5.6\pi \cdot 10^6 \text{ rad} \cdot \text{s}^{-1} / \text{Oe}$$



Permeability spectra of SrM-1 puck  
calculated using Polder's model



# Self-biased circulators: 1<sup>st</sup> run

## ➤ 1<sup>st</sup> run: comparison between SrM-1 and SrM-2

### ➤ Realization

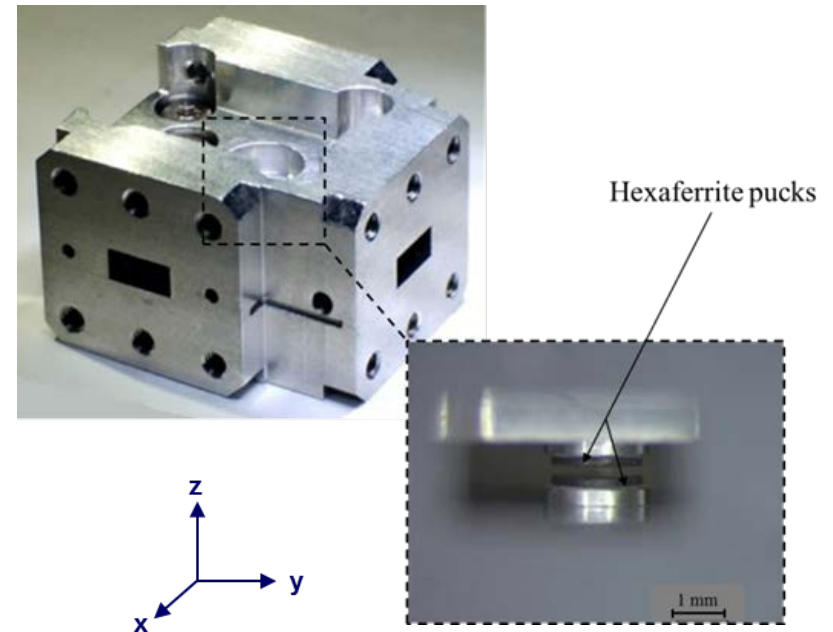
- Y-junction in rectangular waveguide technology (WR-19)
- Hexaferrite machining (c-axis perpendicular to the plane)
- Sticking at the center of the Y-junction

### ➤ Measurement

- Microwave measurement around 40 GHz
- TRL calibration
- Measurement in isolator mode (load connected to one of the port)
- Static magnetic field applied with an electromagnet (when needed)

### ➤ Retro-simulations

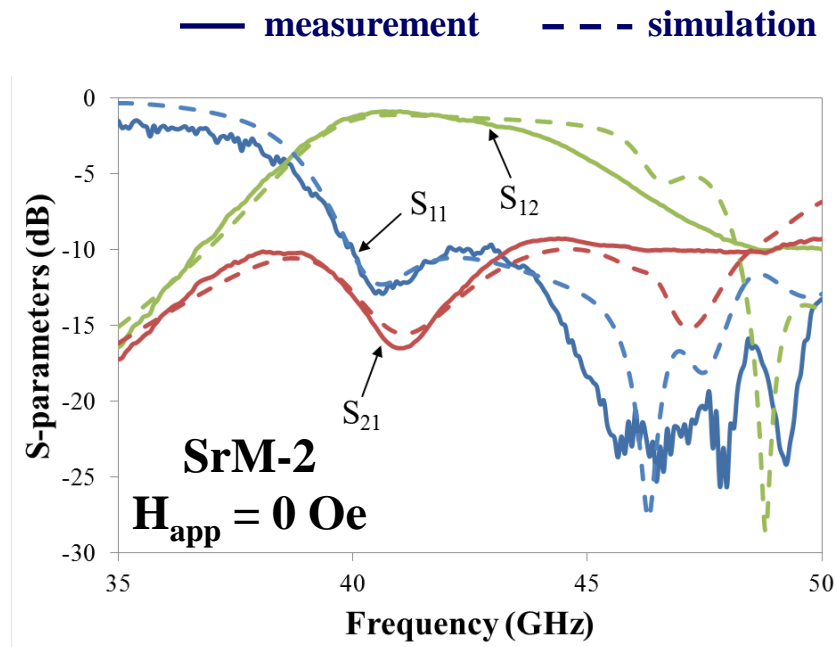
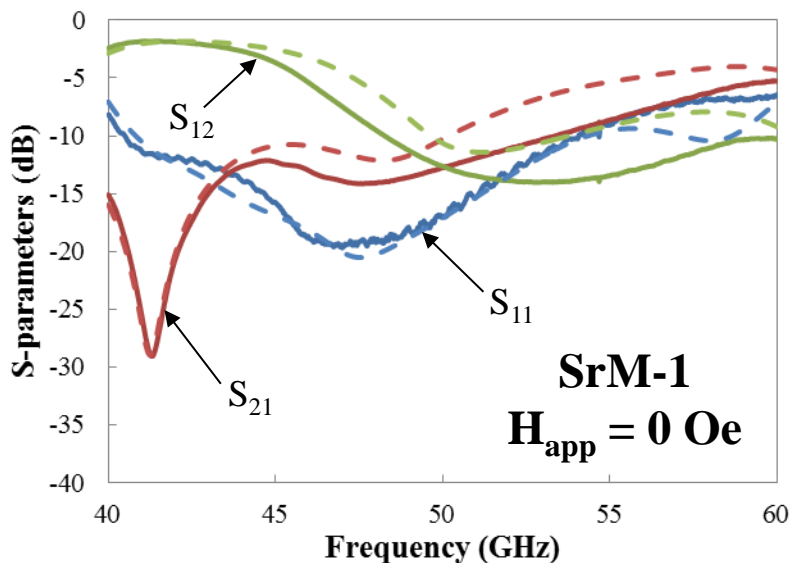
- Evaluate the material properties ( $\Delta H$ ,  $H_k$ )



Photograph of the circulator in rectangular waveguide technology (Insert: hexaferrite pucks placed in the middle of the Y-junction)

# Self-biased circulators: 1<sup>st</sup> run

## Measurements without applied field

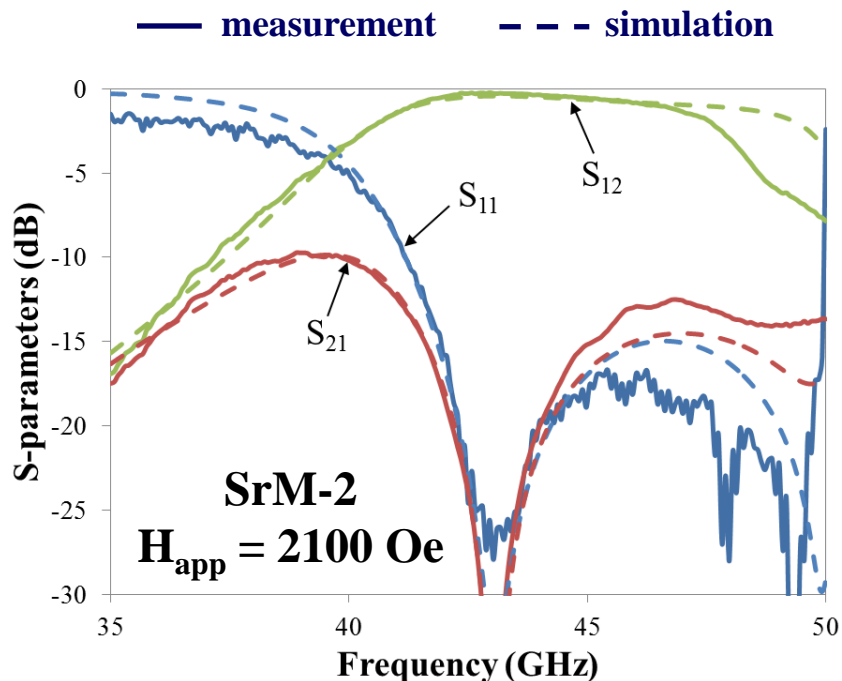
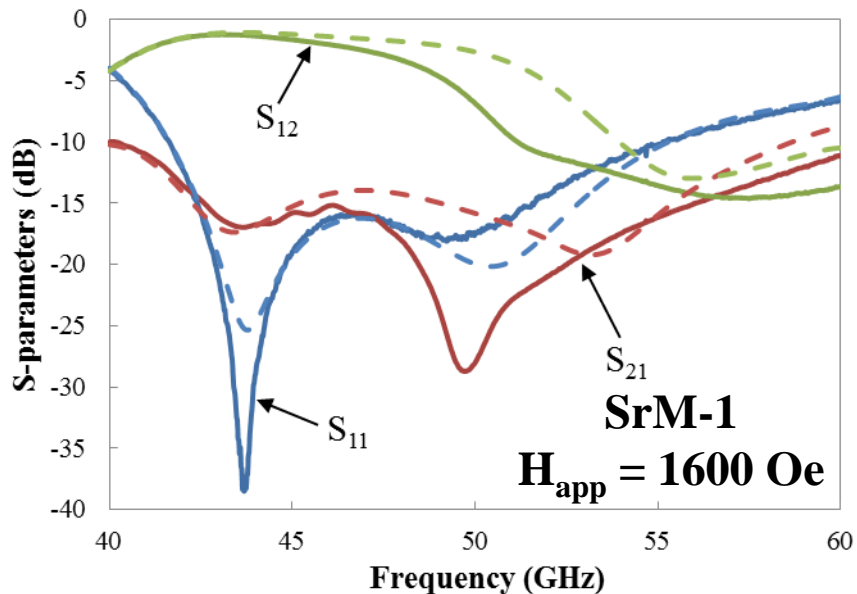


Material	$IL_{min}$ (dB) @f GHz	Isolation (dB)	Adaptation (dB)	$BPR_{Iso < -15dB}$ (%)
SrM-1	1,79 @41,4 GHz	28,1	12,5	7,2
SrM-2	0,87 @41 GHz	16,5	12,6	3,2

- Good agreements between retro-simulations and measurements
- Quite similar working frequencies
- $IL_{SrM-1} = 2 \times IL_{SrM-2}$

# Self-biased circulators: 1<sup>st</sup> run

## Measurements with applied field



Material	$IL_{min}$ (dB) @f GHz	Isolation (dB)	Adaptation (dB)	$BPR_{Iso < -15dB}$ (%)
SrM-1	1,23 @43,2 GHz	16,5	24,6	11,2
SrM-2	0,21 @42,9 GHz	41,3	25,6	9,7

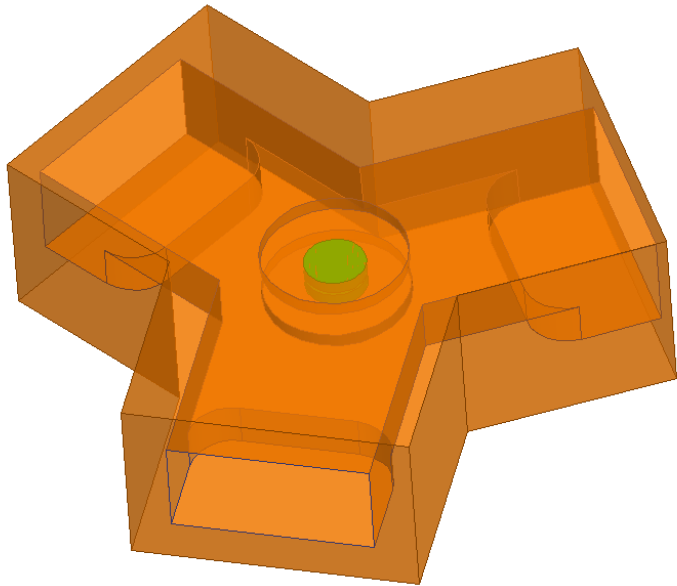
- Performances improvement with a low applied field (Y-junction dimensions can be optimized)
- SrM-2: best candidate ( $\Delta H$  3 times lower than those of SrM-1)

# Self-biased circulators: 2<sup>nd</sup> run

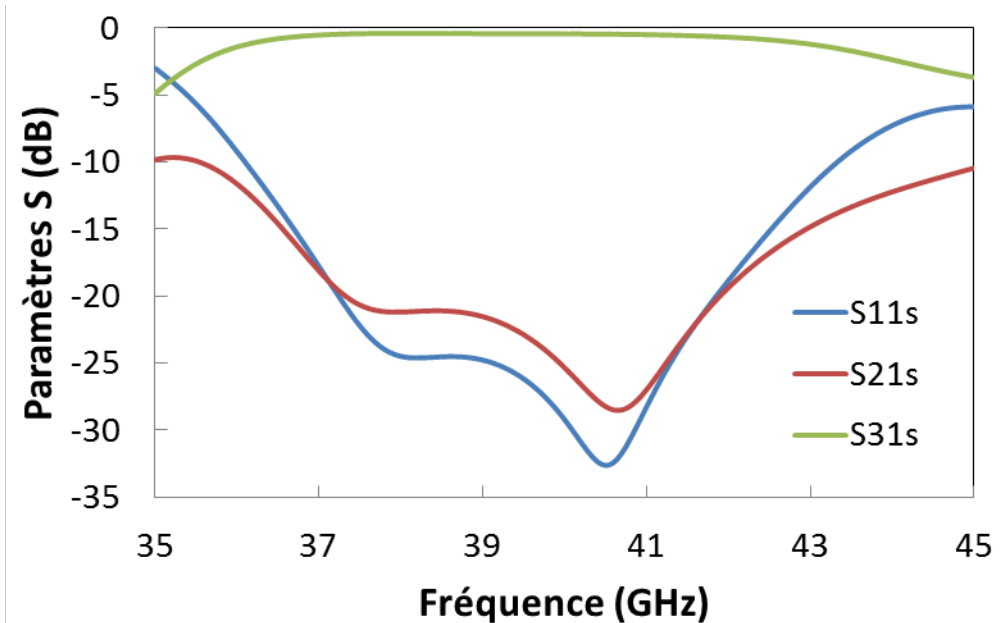
➔ SrM-2 properties:

$M_s$ (G)	$H_k$ (kOe)	$M_r/M_s$	$\Delta H$ (Oe)	$\epsilon_r$
4240	19.75	0.88	<b>400</b>	21

➔ Y-junction optimization:



Optimized structure

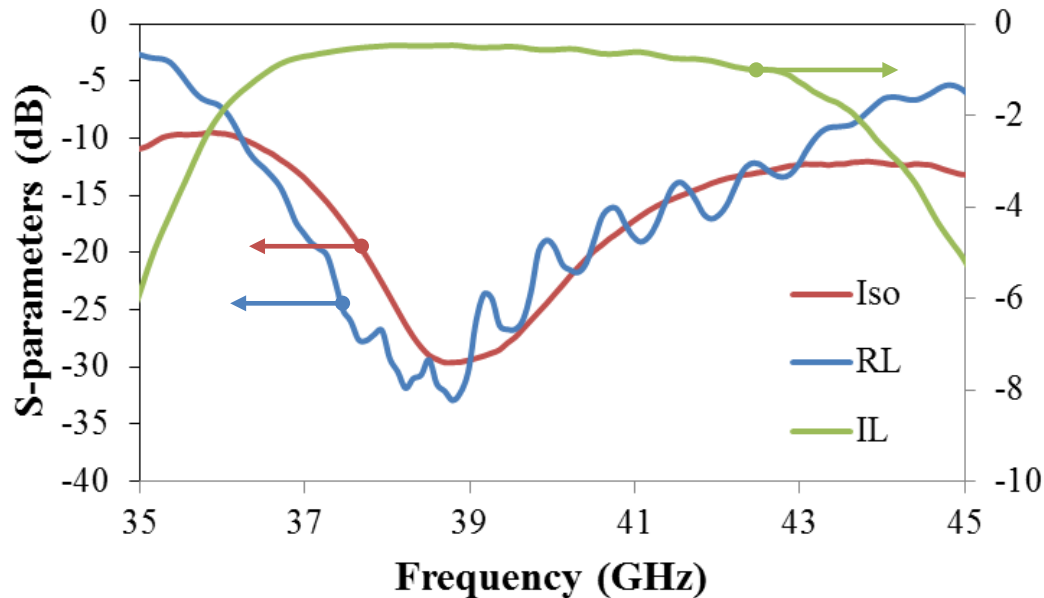


Simulated optimized performances of SrM-2-based circulator

$H_{app}$ (Oe)	$IL_{min}$ (dB) @f GHz	Isolation (dB)	RL (dB)	$RBW_{Iso < -15dB}$ (%)
0	0.41 @38.1 GHz	21.2	24.6	16.9

# Self-biased circulators: 2<sup>nd</sup> run

## ➤ Microwave measurement



$IL_{\min}$ (dB) @ f GHz	0,41 @ 38,9 GHz
Isolation (dB)	26,5
RL (dB)	30,7
$RBW_{Iso < -15 \text{ dB}}$ (%)	10,4

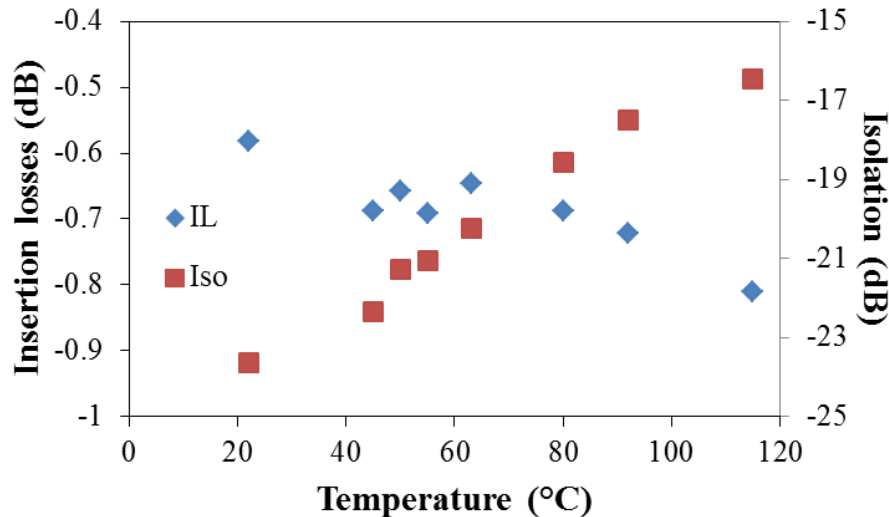
⇒  $IL_{\max}$  in BW = 0,52 dB

⇒ Ripple = 0,11 dB

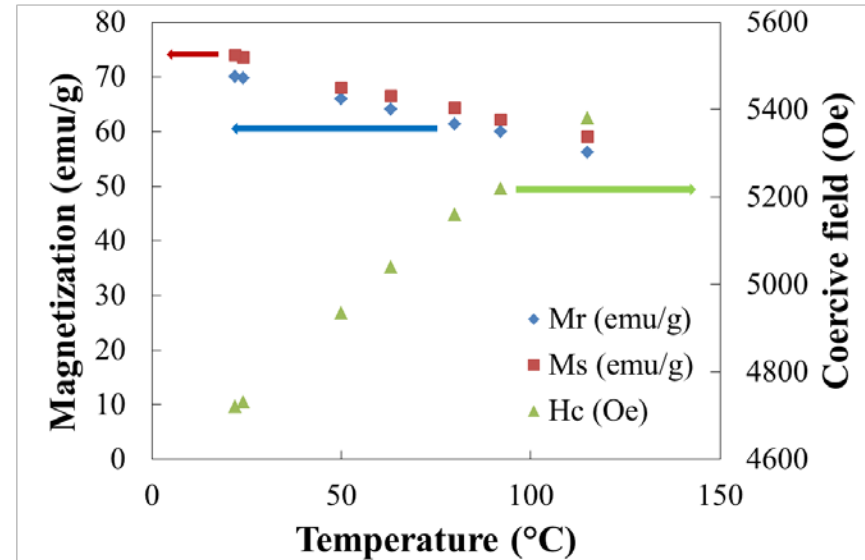
- Significant improvement compared to 1<sup>st</sup> run
- Hexaferrites: competitive / spinel ferrites

# Self-biased circulators: 2<sup>nd</sup> run

## Effect of temperature



Isolation and insertion losses at 40 GHz as a function of temperature

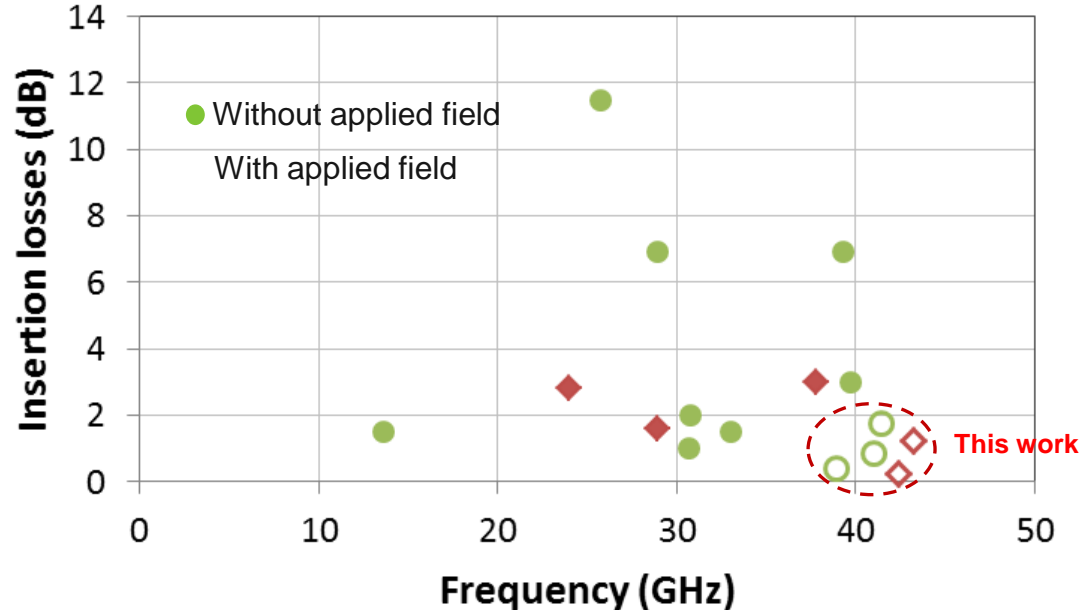


Magnetization and coercive field as a function of temperature

- @ 40 GHz & 115°C:  $\Delta IL = 0.23$  dB,  $\Delta iso = 7$  dB
- Isolation remains > 15 dB up to 115°C
- Decrease of  $M_s$  and  $M_r = 20\%$
- Increase of  $H_c = 14\%$
- **Retro-simulations: linear increase of  $\Delta H$  as a function of temperature ( $\Delta H_{22^\circ C} = 400$  Oe and  $\Delta H_{115^\circ C} = 760$  Oe)**

# Conclusions and prospects

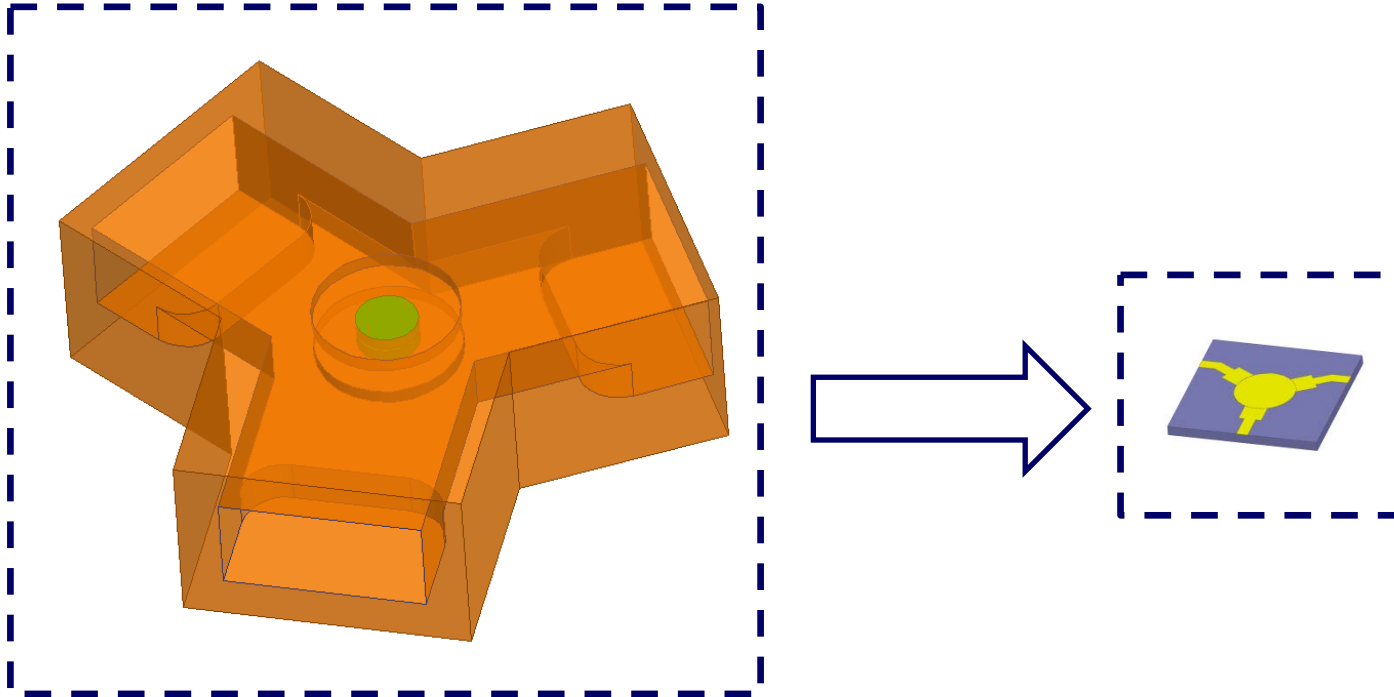
- Selection of a lanthanum-cobalt substituted strontium hexaferrite for mm-wave applications
- Best performances without applied field: IL = 0.41 dB @ 38.9 GHz, RBW = 10.4% (4 GHz)
- Measurements vs temperature: quite good stability



*Insertion losses as a function of frequency measured on hexaferrite-based circulators*

# Conclusions and prospects

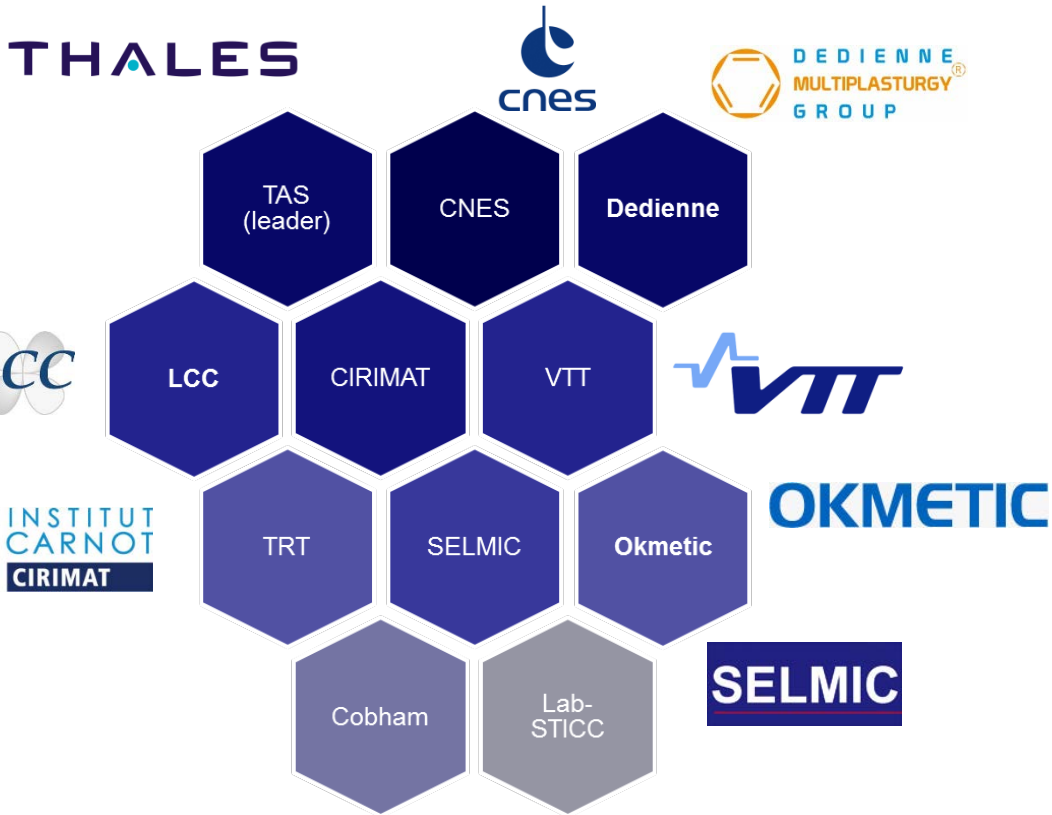
➔ Realization of integrated mm-wave self-biased circulators and isolators



➤ Measured performances at a next SPCD...



# Acknowledgements



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# Thank you for your attention